

## Effect of Ionizing Radiation on the Silicon IMPATT Diode Characteristics

M. B. TAGAEV

*Karakalpak Berdakh State University  
Nukus-UZBEKISTAN*

Received 10.09.1997

### Abstract

We investigated the effect of  $^{60}\text{Co}$   $\gamma$ -irradiation (doses from  $10^2$  to  $2 \times 10^6$  Gy), both without and with heat annealing, on silicon IMPATT diode parameters. It is shown that such treatments improve the diode characteristics (particularly decrease the reverse current and increase both the output and the diffusion length of the minority charge carriers) due to radiation-enhanced processes.

### 1. Introduction

At present a number of technological procedures are known that enable to purposefully change the parameters of device structures based on different semiconductor materials [1-4]. Various methods of gattering and structural - impurity ordering have been developed that can improve the device structure parameters [2, 3]. During manufacturing devices often accumulate various structural defects generated in them during chip formation, dissipative welding and/or thermocompression bonding. This results in both degradation of parameters in the finished product and yield reduction. For such devices the restoration of their properties poses a problem. Conventional heat treatment would not do in this case because the annealing temperature is limited (as the contacts must not be fused). To apply other treatments, one has to know with certainty the nature of the defect as well as the treatment peculiarities, themselves neither of which is often taken into account in practice.

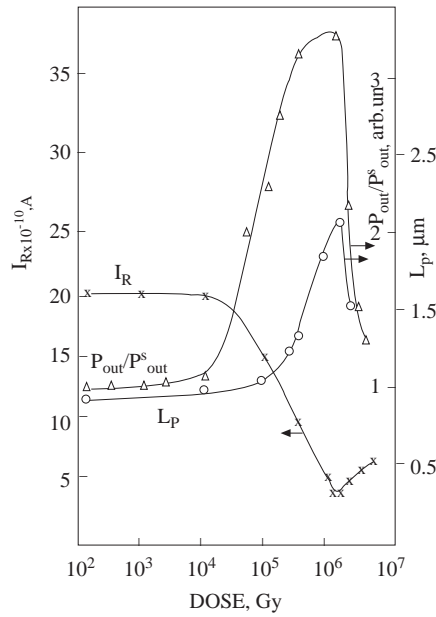
We did manage to improve the parameters of silicon impact-avalanche and transit-time (IMPATT) diodes by  $\gamma$ -irradiation of finished production (packaged diodes) or generator units (IMPATT diodes in a cavity), both with and without heat annealing. Such treatments do not generate structural defects, nor do they result in material compensation and widening of the space charge region (SCR) [1, 5].

## 2. Experimental Procedure

The diodes studied were fabricated using boron diffusion from vapor phase into the  $n - n^+$  Si substrate (the charge carrier concentration in the  $n$  layer was  $(3 + 5) \times 10^{16} \text{ cm}^{-3}$ ). The reverse mesa diameter was  $5 \times 10^{-3} \text{ cm}$ , and the avalanche-breakdown voltage  $V_B$  was 19-20 V. The starting microwave output  $P_{out}^*$  did not exceed 35 mW at operating current  $I_{op} = 100 \text{ mA}$ . The reverse branches of  $I - V$  curves were taken and the diffusion length of minority charge carriers  $L_p$  and output  $P_{out}$  were measured both before and after the corresponding treatments. To treat the diodes studied we used  $^{60}\text{Co}$   $\gamma$ -radiation (doses from  $10^2$  to  $2 \times 10^6 \text{ Gy}$ , dose rate  $3 \text{ Gy/s}$ ), both with and without heat annealing, at temperature  $T = 200\text{-}250^\circ\text{C}$  for 40-60 min.

## 3. Experimental Results and Discussion

Shown in Figure are the dose dependencies of the reverse current  $I_R$  (at the reverse bias  $V_R = 0.9 \text{ V}$ ), diffusion length  $L_p$  and the relative change of the mean microwave output,  $P_{out}/P_{out}^*$ . One can see that both  $I_R$  and  $L_p$  dose dependencies correlate with change of  $P_{out}/P_{out}^*$  change due to  $^{60}\text{Co}$   $\gamma$ -irradiation. According to [6],



**Figure 1.** Dependencies of the silicon IMPATT diode parameters on the absorbed dose of  $^{60}\text{Co}$   $\gamma$ -irradiation: 1- Reverse current  $I_R$ ; 2- Diffusion length of the minority charge carriers  $L_p$ ; 3- Output  $P_{out}$ .

$$P_{out} = (\Delta T w / \epsilon V_B R_T S^{1/2})^2 \mu_{eff} \rho_B, \quad (1)$$

where  $\Delta T$  is the difference between the temperatures of the SCR and the ambient,  $w$  is the SCR width,  $\epsilon$  is permittivity of the diode material,  $R_T$  is the diode heat resistance,  $S$  is the  $p-n$  junction area,  $\mu_{eff}$  is the effective mobility of charge carriers and  $\rho_B$  is the diode resistivity.

From Expression (1) it is evident that if  $w$ ,  $V_B$  and  $\rho_B$  remain constant, then the  $P_{out}$  increase due to  $^{60}\text{Co}$   $\gamma$ -irradiation may result from changes in  $R_T$ ,  $S$  and/or  $\mu_{eff}$ . Indeed, the direct heat resistance measurements for the IMPATT diodes studied have shown that  $R_T$  was decreasing during  $\gamma$ -irradiation. This results from the increase of the effective cross section area of the active region where heat dissipation occurred. In addition, the effective mobility  $\mu_{eff}$  may grow as a result of the radiation-enhanced gettering due to a decrease in the number of scattering centers. The last statement is circumstantially evidenced by the results of direct electron-probe measurements of the diffusion length  $L_p$  both before and after  $\gamma$ -irradiation of test structures fabricated from the same wafers that were used to fabricate the IMPATT diodes studied (see Figure, curve 2).

We have studied also the effect of the low-temperature ( $T = 200\text{-}280^\circ\text{C}$ ) annealing on the output  $P_{out}$  and the reverse current  $I_R$  for the IMPATT diodes preirradiated by the  $^{60}\text{Co}$   $\gamma$ -quanta. The corresponding results are given in Tables 1-3.

**Table 1.** Effect of  $^{60}\text{Co}$   $\gamma$ -irradiation (without and with heat annealing at  $200^\circ\text{C}$  for 1 hour) on the  $P_{out}/P_{out}^*$  and  $I_R/I_R^S$  ratios for silicon IMPATT diodes.

Irradiation dose Gy	Without heat annealing		With heat annealing	
	$P_{out}/P_{out}^S$	$I_R/I_R^S$	$P_{out}/P_{out}^S$	$I_R/I_R^S$
$1 \times 10^2$	1.00	1.00	1.00	1.00
$5 \times 10^2$	1.00	1.00	1.06	1.00
$1 \times 10^3$	1.05	1.00	1.10	1.00
$1 \times 10^4$	1.66	1.00	1.82	0.50
$1 \times 10^5$	2.61	0.75	3.01	0.32
$5 \times 10^5$	2.93	0.50	3.93	0.28
$7 \times 10^5$	3.12	0.35	4.12	0.20
$1 \times 10^6$	1.54	0.25	3.07	0.32
$2 \times 10^6$	1.54	0.20	1.00	0.70

**Table 2.** Effect of the temperature of heat annealing (for 1 hour) on the  $P_{out}/P_{out}^S$  and  $I_R/I_R^S$  ratios for  $^{60}\text{Co}$   $\gamma$ -irradiated (dose of  $5 \times 10^5$  Gy) silicon IMPATT diodes.

Diode No:	Temperature of heat annealing, $^\circ\text{C}$	Before heat annealing		After heat	
		$P_{out}/P_{out}^S$	$I_R/I_R^S$	$P_{out}/P_{out}^S$	$I_R/I_R^S$
1	100	2.90	0.50	2.90	0.45
2	140	2.90	0.37	3.13	0.15
3	180	2.90	0.37	3.50	0.14
4	200	2.90	0.28	3.91	0.12
5	250	2.90	0.35	3.74	0.10
6	280	2.90	0.37	3.02	0.12

**Table 3.** Effect of the duration of heat annealing (at 200°C) on the  $P_{out}/P_{out}^S$  and  $I_R/I_R^S$  ratios for  $^{60}\text{Co}$   $\gamma$ -irradiated silicon IMPATT diodes (dose of  $7 \times 10^5$  Gy).

Diode No:	Duration of heat annealing, min	Before heat annealing		After heat annealing	
		$P_{out}/P_{out}^S$	$I_R/I_R^S$	$P_{out}/P_{out}^S$	$I_R/I_R^S$
1	20	3.02	0.50	3.02	0.50
2	40	3.02	0.40	3.76	0.19
3	60	3.02	0.40	4.09	0.12
4	80	3.02	0.45	3.81	0.16
5	100	3.02	0.35	3.59	0.17
6	120	3.02	0.35	3.43	0.20

One can see that the low-temperature annealing after  $^{60}\text{Co}$   $\gamma$ -irradiation increases  $P_{out}$  as well. It should be noted that the above heat treatment of the non-irradiated IMPATT diodes either resulted in a decrease of the output  $P_{out}$ , or, at best, did not change it.

#### 4. Conclusion

Thus it may be concluded that  $^{60}\text{Co}$   $\gamma$ -irradiation (doses up to  $10^6$  Gy) of silicon IMPATT diodes may lead to the improvement of their respective parameters. In particular, the output is increased due to the radiation-enhanced processes in the device active area. Introduction of such a technological procedure into manufacturing of such devices will result in a yield rise.

#### References

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